

REMARKS

Claims 1-42 are pending. Claims 1-12, 14-19, 21-36, and 39-41 have been amended to avoid multiply dependent claims. Applicants respectfully request that the amendments and remarks made herein be entered and made of record in the file history of the present application.

No fee is believed to be due for this amendment. Should any fee be required, please charge same to Deposit Account No. 16-1150.

Respectfully submitted,

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Charles E. Miller

24,576
(Reg. No.)

PENNIE & EDMONDS LLP
1155 Avenue of the Americas
New York, New York 10036-2711

(212) 790-9090

APPENDIX A

1.(amended) Process for **[the preparation of] preparing** a composition **[comprising] of** a vinylaromatic polymer matrix surrounding rubber nodules, comprising **[a] the** step of polymerizing at least one vinylaromatic monomer in the presence of a rubber, **[of]** a stable free radical which is not introduced into the polymerization mixture in a form linked to the rubber, and **[of]** a polymerization initiator with a grafting character suitable for **[the]** said composition,

[- is such that in one of its sections at least 90% of the total area occupied by the nodules corresponds to capsules having an equivalent diameter ranging from 0.1 to 1 μm , or else

- is such that it comprises multi-occlusion-type nodules and is such that in one of its sections

- 20 to 60% of the total are occupied by the particles corresponds to particles having an equivalent diameter ranging from 0.1 to 1 μm ,

- 5 to 20% of the total area occupied by the particles corresponds to particles having an equivalent diameter ranging from 1 to 1.6 μm , and

- 20 to 75% of the total area occupied by the particles corresponds to particles having an equivalent diameter of greater than 1.6 μm .

the] said step being such that:

- if (SFR) represents the number of moles of stable free radical in the polymerization mixture,

- if F_{SFR} represents the functionality of the stable free radical, i.e. the number of sites on the same molecule of stable free radical having the stable free radical state,

- if (INIT) represents the number of moles of polymerization initiator in the polymerization mixture before phase inversion, and

- if F_{INIT} represents the functionality of the initiator introduced before phase inversion, i.e. the number of sites having the free radical state that each molecule of initiator is capable of generating, then:

$$0.05 < \frac{F_{\text{SFR}} \times (\text{SFR})}{F_{\text{INIT}} \times (\text{INIT})} < 1.$$

2. (amended) Process according to **[the previous claim] claim 1**, characterized in that

$$0.05 < \frac{F_{\text{SFR}} \times (\text{SFR})}{F_{\text{INIT}} \times (\text{INIT})} < 0.5.$$

3. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that, if (RU) represents the number of moles of rubber,

$$0.1 < \frac{(\text{SFR}) \times F_{\text{SFR}}}{(\text{RU})} < 10.$$

4. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the ratio of (INIT) x F_{INIT} to the molar amount of vinylaromatic monomer ranges from 1 x 10⁻⁵ to 1 x 10⁻².

5. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the ratio of (INIT) x F_{INIT} to the molar amount of vinylaromatic monomer is greater than 2 x 10⁻⁴.

6. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the ratio of (INIT) x F_{INIT} to the molar amount of vinylaromatic monomer is greater than 4 x 10⁻⁴.

7. (amended) Process according **[one of the preceding claims] claim 1**, characterized in that the ratio of (INIT) x F_{INIT} to the molar amount of vinylaromatic monomer is greater than 6 x 10⁻⁴.

8. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization mixture during the step of the process comprises, per 100 parts by weight of vinylaromatic monomer, 2 to 35 parts by weight of rubber and 0 to 5 parts by weight of solvent.

9. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the rubber has a weight-average molecular mass ranging from 110,000 to 350,000 and a number-average molecular mass ranging from 50,000 to 250,000, and in that the matrix of vinylaromatic polymer has a weight-average molecular mass ranging from 90,000 to 250,000.

10. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the rubber nodules have partially both a salami and/or labyrinth morphology and partially both an onion and/or capsule morphology.

11. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the composition is such that, in one of its sections,

- 20 to 60% of the total area occupied by the particles corresponds to particles having an equivalent diameter ranging from 0.1 to 1 μm ,
- 5 to 20% of the total area occupied by the particles corresponds to particles having an equivalent diameter ranging from 1 to 1.6 μm , and
- 20 to 75% of the total area occupied by the particles corresponds to particles having an equivalent diameter of greater than 1.6 μm .

12. (amended) Process according to **[the preceding claim] claim 11**, characterized in that:

- in the 0.1 to 1 μm size range, more than 95% of the particles have the salami or capsule morphology,
- in the 1 to 1.6 μm size range, more than 95% of the particles have the salami morphology, and
- in the greater than 1.6 μm size range, more than 95% of the particles have the salami morphology.

13. Process according to claim 11, characterized in that

- in the 0.1 to 1 μm size range, more than 95% of the particles have the capsule or onion or labyrinth morphology,

- in the 1 to 1.6 μm size range, more than 95% of the particles have the onion or labyrinth morphology, and

- in the greater than 1.6 μm size range, more than 95% of the particles have the labyrinth morphology.

14. (amended) Process according to **[one of the preceding claims]** **claim 1**, characterized in that the distribution of the equivalent diameters of nodules is bimodal.

15. (amended) Process according to **[one of Claims 10 to 14]** **claim 10**, characterized in that the rubber has, as a 5% by weight solution in styrene, a viscosity at 25°C ranging from 60 to 300 mPa.s.

16. (amended) Process according to **[one of Claims 10 to 15]** **claim 10**, characterized in that the rubber has a weight-average molecular mass ranging from 175,000 to 350,000 and a number-average molecular mass ranging from 70,000 to 250,000.

17. (amended) Process according to **[the preceding claim]** **claim 16**, characterized in that the rubber has a weight-average molecular mass ranging from 200,000 to 300,000 and a number-average molecular mass ranging from 90,000 to 200,000.

18. (amended) Process according to **[one of Claims 1 to 9]** **claim 1**, characterized in that the composition is such that, in one of its sections, at least 90% of the total area occupied by the particles corresponds to capsules having an equivalent diameter ranging from 0.1 to 1 μm .

19. (amended) Process according to **[the preceding claim]** **claim 18**, characterized in that the rubber has, as a 5% by weight solution in styrene, a viscosity at 25°C ranging from 15 to 60 mPa.s.

20. Process according to Claim 18 or 19, characterized in that the rubber has a weight-average molecular mass ranging from 110,000 to 200,000 and a number-average molecular mass ranging from 50,000 to 200,000.

21. (amended) Process according to **[the preceding claim] claim 20**, characterized in that the rubber has a weight-average molecular mass ranging from 150,000 to 200,000 and a number-average molecular mass ranging from 70,000 to 150,000.

22. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the rubber is a homopolybutadiene.

23. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the initiator is one of the following:

- isopropyl *tert*-butyl peroxy carbonate,
- 2-ethylhexyl *tert*-butyl peroxy carbonate,
- dicumyl peroxide
- di-*tert*-butyl peroxide,
- 1,1-bis(*tert*-butylperoxy)cyclohexane,
- 1,1-bis(*tert*-butylperoxy)-3,3,5- trimethylcyclohexane,
- *tert*-butyl peroxyacetate,
- cumyl *tert*-butyl peroxide,
- *tert*-butyl perbenzoate,
- *tert*-butyl per-2-ethylhexanoate,
- 2,2-bis(*tert*-butylperoxy)butane,
- butyl 4,4-bis(*tert*-butyl)valerate,
- ethyl 3,3-bis(*tert*-butyl)butyrate,
- 2,2-bis(4,4-di-*tert*-butylperoxycyclo-

hexyl)propane.

24. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the initiator is chosen from diacyl peroxides, peroxy esters, dialkyl peroxides and peroxy acetals.

25. (amended) Process according to **[the preceding claim] claim 24**, characterized in that the initiator generates at least one *tert*-butoxy radical.

26. (amended) Process according to **[the preceding claim] claim 25**, characterized in that the initiator is one of the following:

- isopropyl *tert*-butyl peroxy carbonate,
- 1,1-bis(*tert*-butylperoxy)cyclohexane,
- 1,1-bis(*tert*-butylperoxy)-3,3,5-trimethyl- cyclohexane.

27. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization step is carried out at least partially at 80 to 140°C.

28. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization step is carried out at least partially at 90 to 130°C.

29. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization step is carried out at least partially, before phase inversion, at a temperature T such that $T_{1/2} - 20^{\circ}\text{C} < T < T_{1/2} + 20^{\circ}\text{C}$, in which $T_{1/2}$ represents the temperature at which 50% of the initiator is decomposed in one hour.

30. (amended) Process according to **[the preceding claim] claim 29**, characterized in that the step is carried out at least partially at a temperature T such that $T_{1/2} - 10^{\circ}\text{C} < T < T_{1/2} + 10^{\circ}\text{C}$.

31. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization initiator is added to the polymerization mixture after phase inversion.

32. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the vinylaromatic monomer is styrene.

33. (amended) Process according to **[one of the preceding claims] claim 1**, characterized in that the polymerization is carried out continuously so that the phase inversion takes place in a plug-flow reactor.

34.(amended) **A [Composition] composition comprising a vinylaromatic polymer matrix surrounding rubber nodules,[capable of being obtained by the process of claim 1]**

- which is such that, in one of its sections, at least 90% of the total area is occupied by the nodules corresponds to capsules having an equivalent diameter ranging from 0.1 to 1 µm, or alternatively

- which comprises multi-occlusion-type nodules and is such that in one of its sections

- **20 to 60% of the total area is occupied by the particles corresponds to particles having an equivalent diameter ranging from 0.1 to 1 µm,**
- **5 to 20% of the total area is occupied by the particles corresponds to particles having an equivalent diameter ranging from 1 to 1.6 µm, and**
- **20 to 75% of the total area is occupied by the particles corresponds to particles having an equivalent diameter of greater than 1.6 µm.**

35. (amended) Composition according to **[the preceding claim or] claim 34** comprising a stable free radical which is in a free form or in a form linked to a polymer chain by a covalent bond, comprising a matrix of vinylaromatic polymer surrounding rubber nodules, characterized in that the composition comprises nodules of the multi-occlusion type and is such that, in one of its sections,

- 20 to 60% of the total area occupied by the particles corresponds to particles having an equivalent diameter ranging from 0.1 to 1 µm,

- 5 to 20% of the total area occupied by the particles corresponds to particles having an equivalent diameter ranging from 1 to 1.6 µm, and

- 20 to 75% of the total area occupied by the particles corresponds to particles having an equivalent diameter of greater than 1.6 µm.

36. (amended) Composition according to **[the preceding claim]** **claim 35**, characterized in that:

- in the 0.1 to 1 μm size range, more than 95% of the particles have the salami or capsule morphology,
- in the 1 to 1.6 μm size range, more than 95% of the particles have the salami morphology, and
- in the greater than 1.6 μm size range, more than 95% of the particles have the salami morphology.

37. Composition according to Claim 35, characterized in that

- in the 0.1 to 1 μm size range, more than 95% of the particles have the capsule or onion or labyrinth morphology,
- in the 1 to 1.6 μm size range, more than 95% of the particles have the onion or labyrinth morphology, and
- in the greater than 1.6 μm size range, more than 95% of the particles have the labyrinth morphology.

38. Composition according to one of Claims 34 to 37, characterized in that the distribution of the equivalent diameters of nodules is bimodal.

39. (amended) Composition according to **[one of Claims 34 to 38]** **claim 34**, characterized in that the melt index at 210°C with 5 kg is greater than 15 g/10 min (ISO 1133 H), the Vicat softening temperature (1 kg) is greater than 94°C (ISO 306 A50) and the notched Izod impact strength is greater than 8 kJ/m² (ISO 180/1A).

40. (amended) Composition according to **[the preceding claim]** **claim 34**, characterized in that the Vicat softening temperature (1 kg) is greater than 94.5°C and the notched Izod impact strength is greater than 9 kJ/m².

41. (amended) Case for a television or a video recorder or a computer or a printer or a fax machine produced by injection moulding a composition of **[one of Claims 35 to 40]** **claim 35**.

42. Composition according to Claim 34, characterized in that the composition is such that, in one of its sections, at least 90% of the total area occupied by the particles corresponds to capsules having an equivalent diameter ranging from 0.1 to 1 μm .